

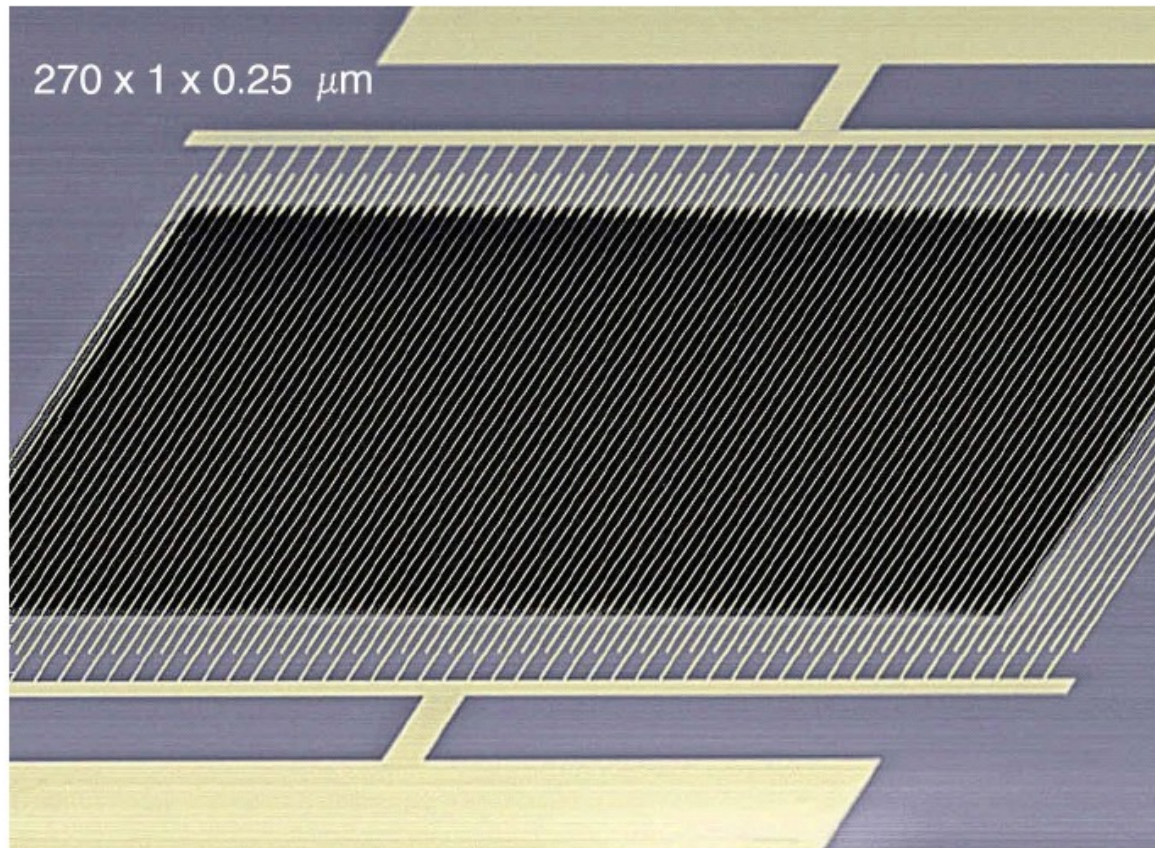
Intrinsic localized modes in microelectromechanical oscillator arrays: a dynamical approach

Qingfei Chen
Arizona State University

Collaboration with
Liang Huang
Ying-Cheng Lai
Arizona State University

Microelectromechanical (MEM) arrays

MEMS device in array structure:



Micro resonator

Micro sensor

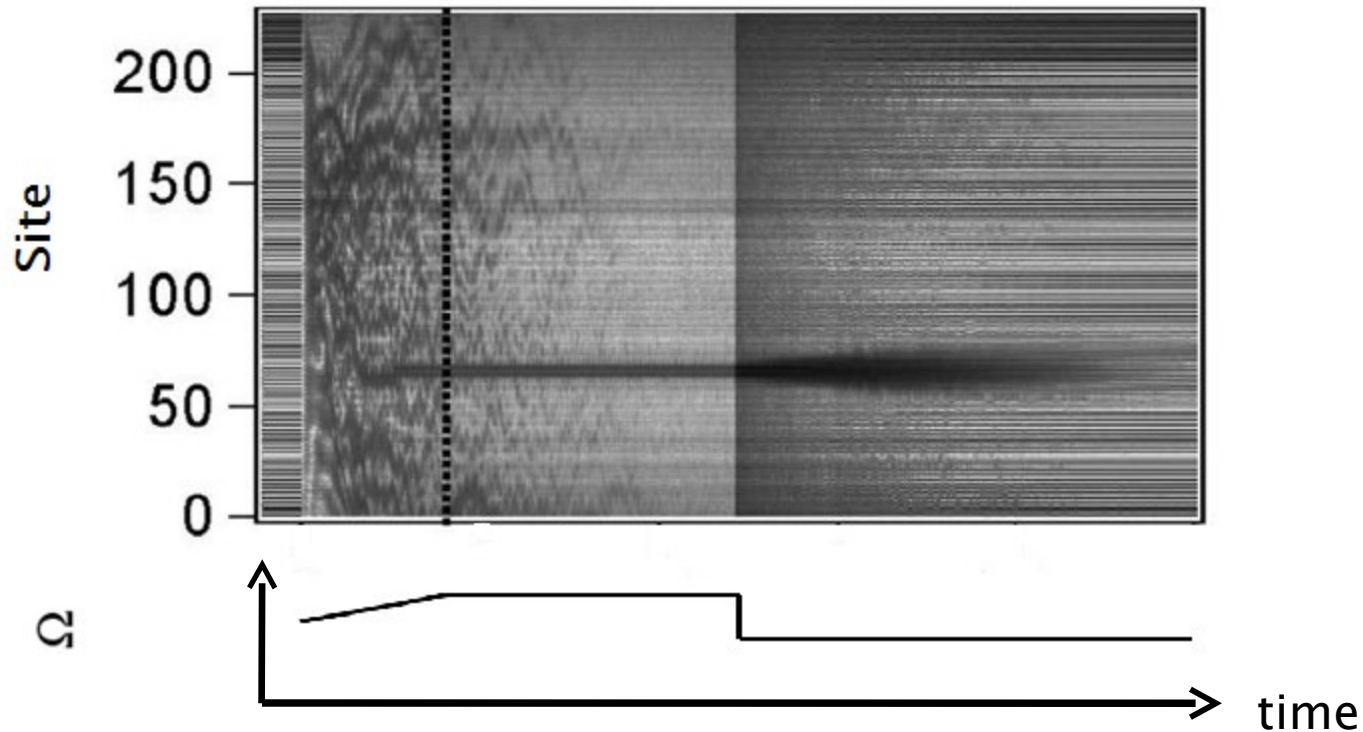
Micro mechanical filter

Micro generator



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-
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E. Buks and M. L. Roukes, J. Microelectromech. Syst., 11, 802 (2002).

Intrinsic localized modes (ILMs) in MEM oscillator array: Experiment

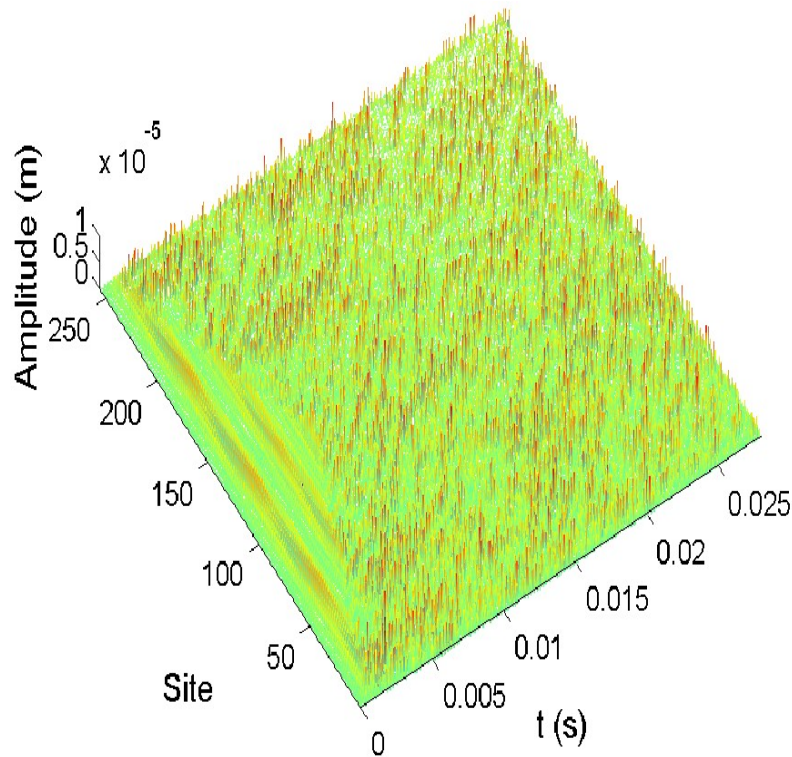


M. Sato et. al., Rev. Mod. Phys. 78, 137 (2006).

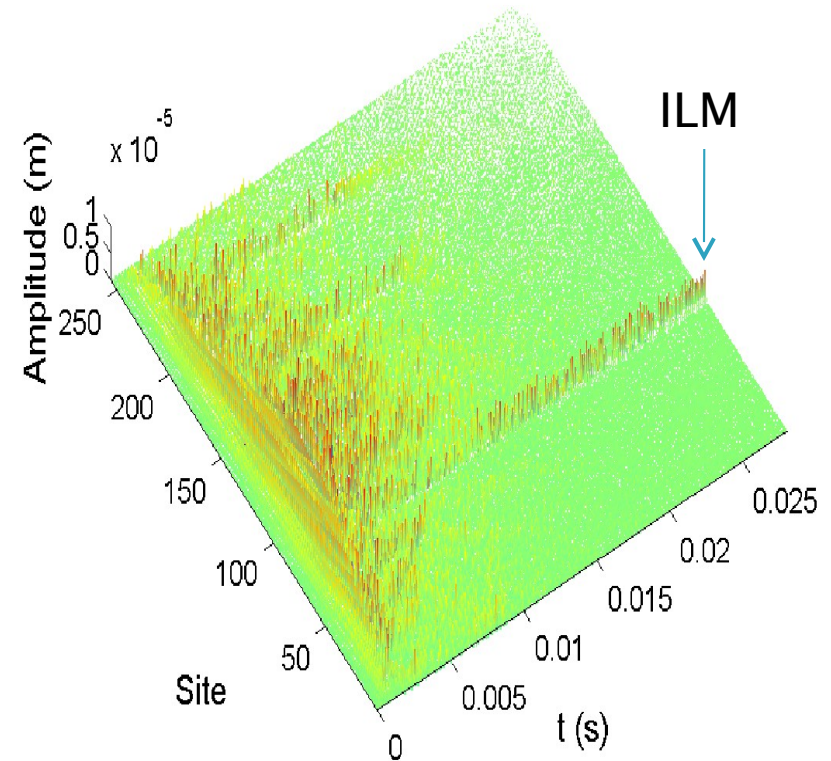
- ▶ The **dynamical mechanism** for ILMs in MEMS was not very clear.

- ▶ We propose a dynamical analysis for **better understanding** of ILMs' creation mechanism.

- ▶ We find that ILMs can be excited from **inherent spatiotemporal chaos**.

Spatiotemporal chaos and intrinsic localized modes in MEM arrays

Inherent spatiotemporal chaos:

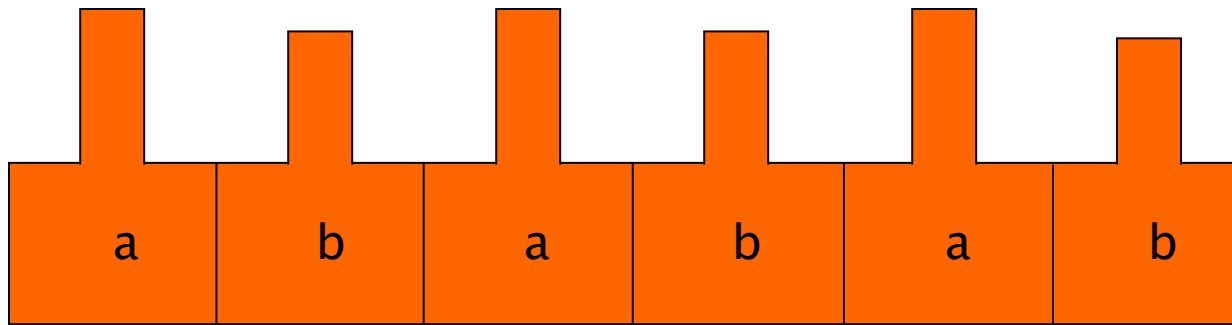


Intrinsic localized mode:



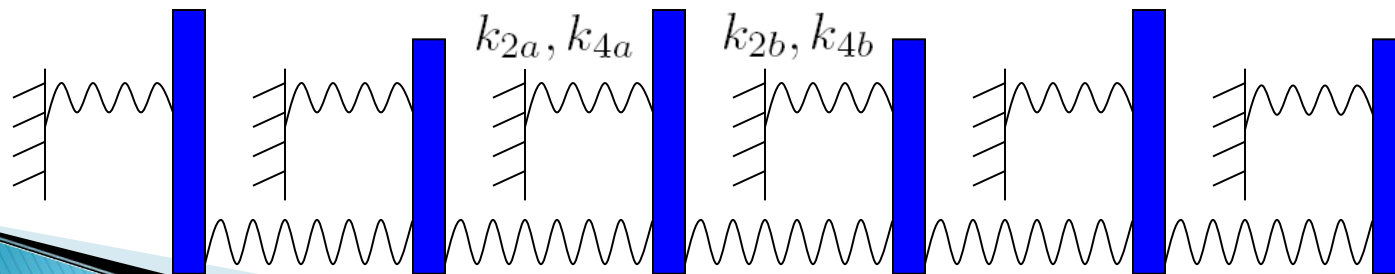
Experimental settings

Cantilever array structure and its equivalent mass-spring model:



k_{2a}, k_{4a} : harmonic and anharmonic spring constants of long beams

k_{2b}, k_{4b} : harmonic and anharmonic spring constants of short beams



k_I k_I : coupling spring constants

Dynamic model of MEM arrays

MEM cantilever arrays equation:

$$m_i \ddot{x}_i + b_i \dot{x}_i + k_{2i} x_i + k_{4i} x_i^3 + k_I (2x_i - x_{i+1} - x_{i-1}) = m_i \alpha \cos(\Omega t),$$

where $x_i (i = 1, 2, \dots, N)$ N is even

$$(m_i, b_i, k_{2i}, k_{4i}) = (m_a, b_a, k_{2a}, k_{4a})$$

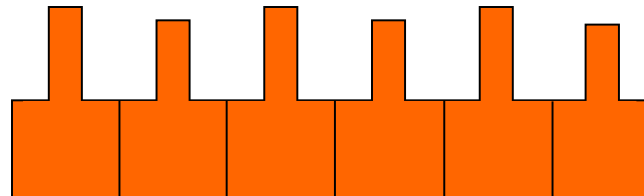
$$= (5.5 \times 10^{-13} \text{ kg}, 6.2 \times 10^{-11} \text{ kg/s}, 0.303 \text{ N/m}, 5 \times 10^8 \text{ N/m}^3) \quad \text{if } i \text{ is odd}$$

$$(m_i, b_i, k_{2i}, k_{4i}) = (m_b, b_b, k_{2b}, k_{4b})$$

$$= (5.0 \times 10^{-13} \text{ kg}, 5.7 \times 10^{-11} \text{ kg/s}, 0.353 \text{ N/m}, 5 \times 10^8 \text{ N/m}^3) \quad \text{if } i \text{ is even}$$

m_i : mass

b_i : damping coefficient



Averaged model for MEM arrays

$$x_i(t) = U_i(t) \cos(\Omega t) + V_i(t) \sin(\Omega t)$$

$$\frac{du_i}{dt} = -\frac{1}{2\Omega} [(\Omega^2 - \Omega_{oi}^2)v_i - \frac{3k_{4i}}{4m_i}v_i(u_i^2 + v_i^2) + \frac{\Omega_{oi}}{Q_i}\Omega u_i - \frac{k_I}{m_i}(2v_i - v_{i+1} - v_{i-1})],$$

$$\frac{dv_i}{dt} = -\frac{1}{2\Omega} [(\Omega^2 - \Omega_{oi}^2)u_i - \frac{3k_{4i}}{4m_i}u_i(u_i^2 + v_i^2) - \frac{\Omega_{oi}}{Q_i}\Omega v_i + \alpha - \frac{k_I}{m_i}(2u_i - u_{i+1} - u_{i-1})],$$

where $\Omega_{oi} = \sqrt{k_{2i}/m_i}$, $Q_i = \sqrt{m_i k_{2i}/b_i}$

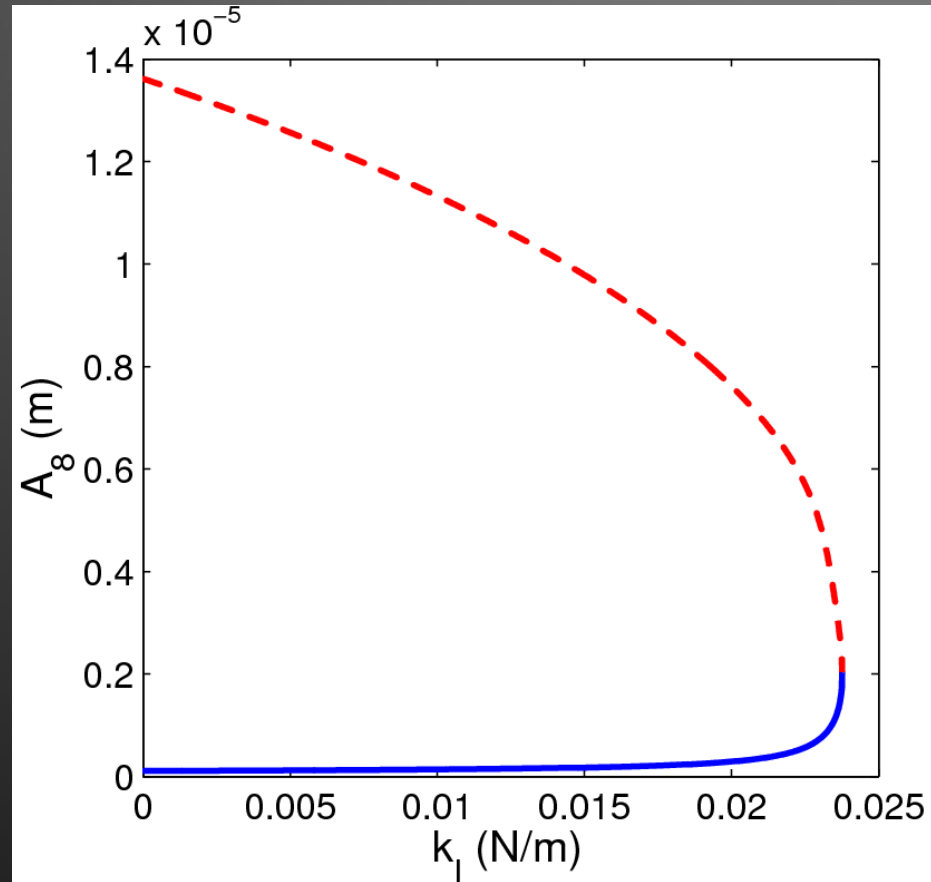
u_i and v_i are the average functions of U_i and V_i over one period.

Amplitudes and phase angles can be approximated by:

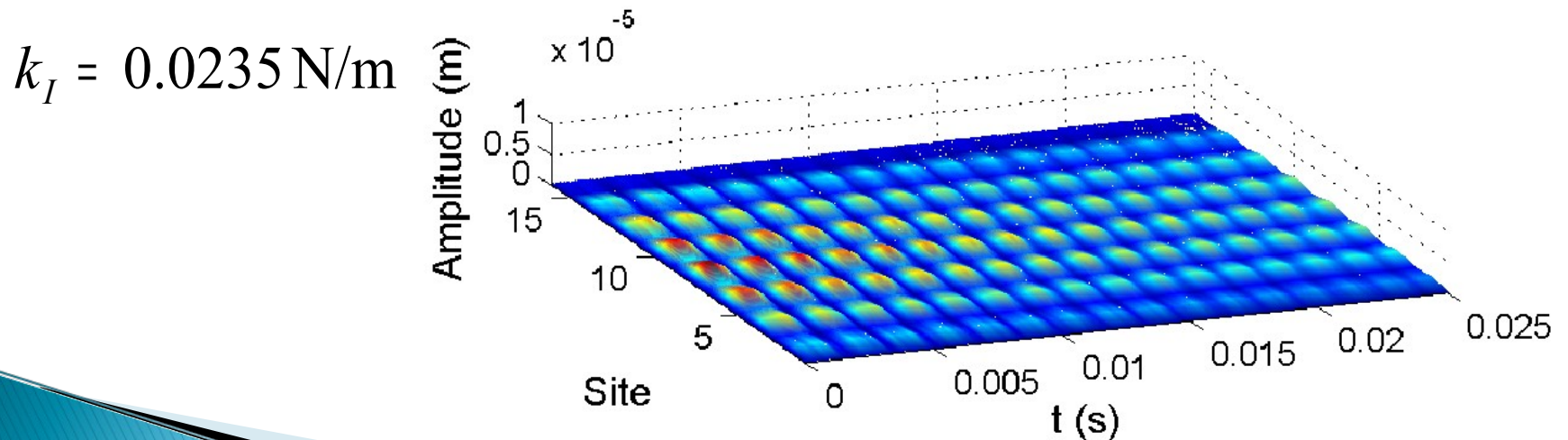
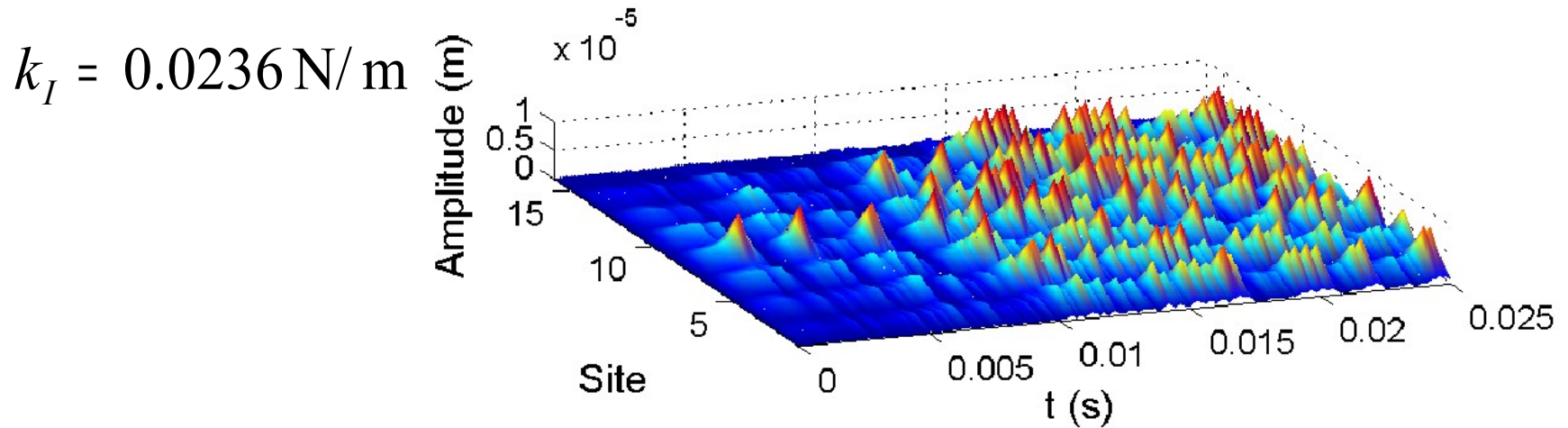
$$A_i = \sqrt{u_i^2 + v_i^2}, \theta_i = \arctan(v_i / u_i)$$

Saddle-node Bifurcation to spatiotemporal chaos

Bifurcation diagram of low energy state in averaged system ($N=16$):



Saddle-node bifurcation to spatiotemporal chaos



Generating ILMs from spatiotemporal (ST) chaos

In the previous literature, people considered that

1 Initial noise

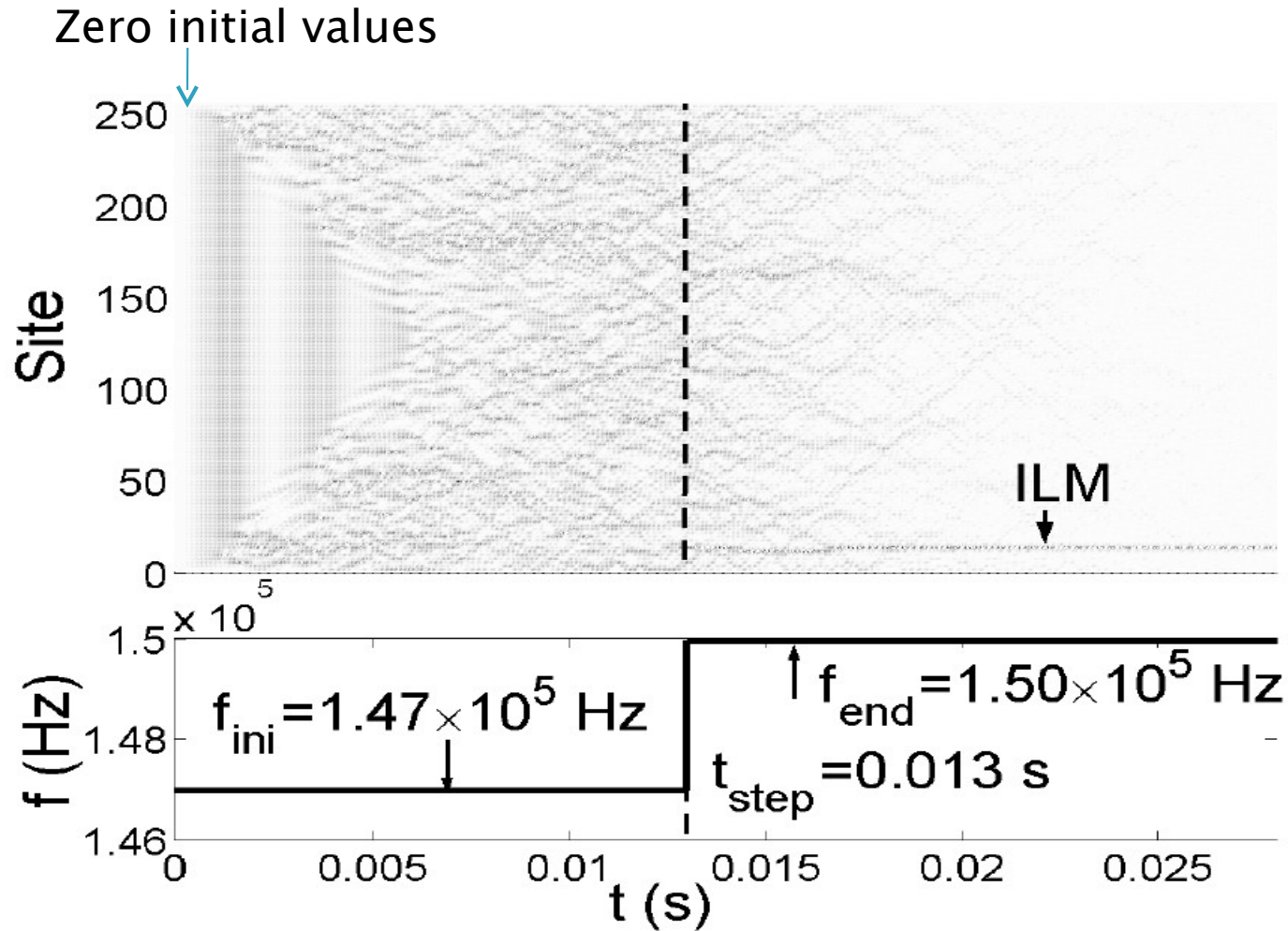
2 Frequency chirping scheme

are necessary for generating ILMs in MEM arrays.

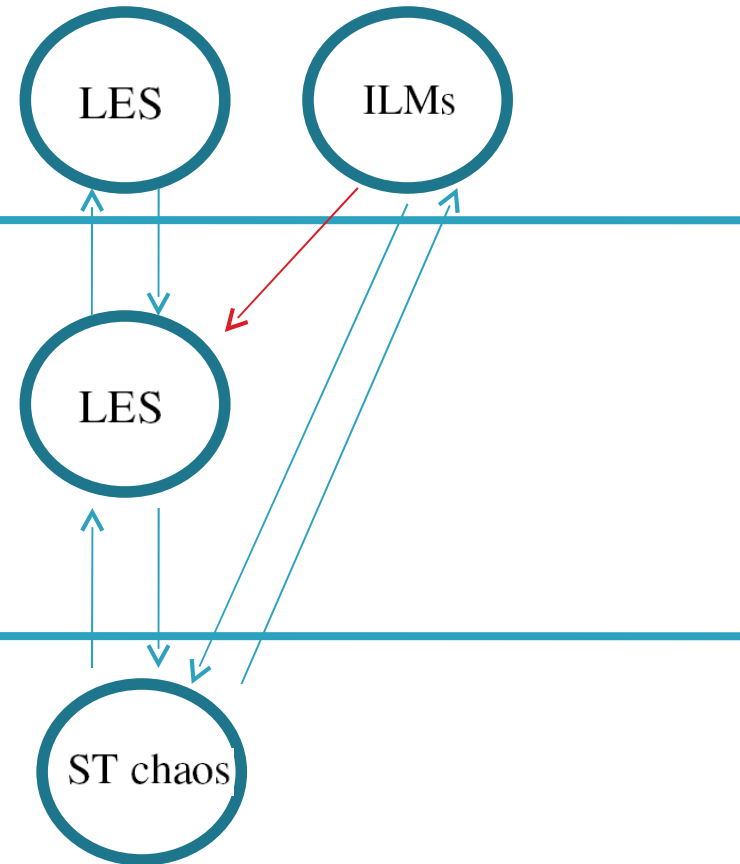
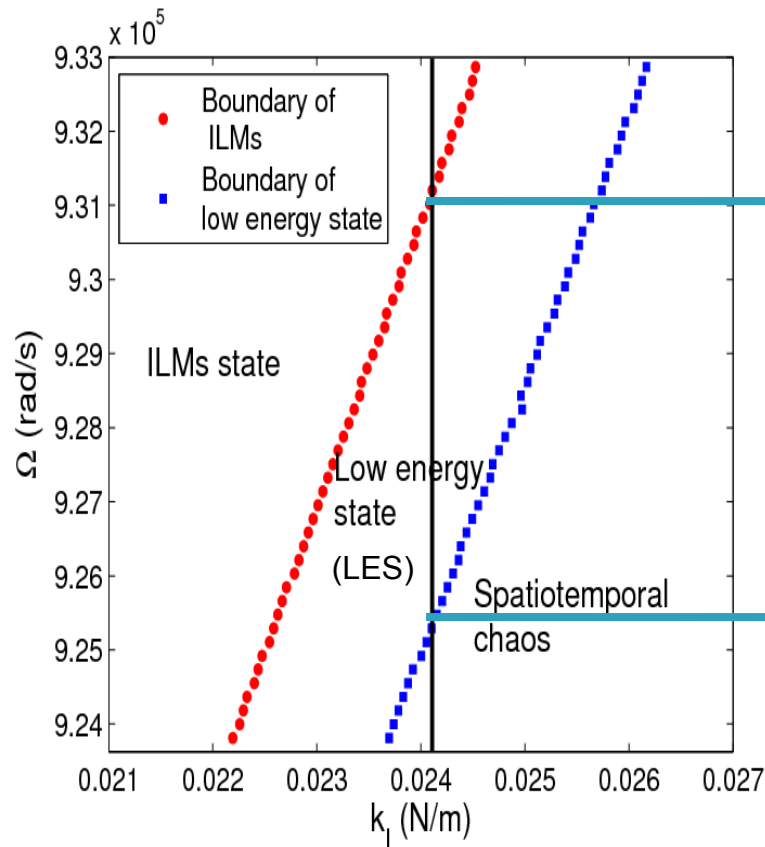
However, due to **inherent ST chaos**, these conditions can be relaxed.

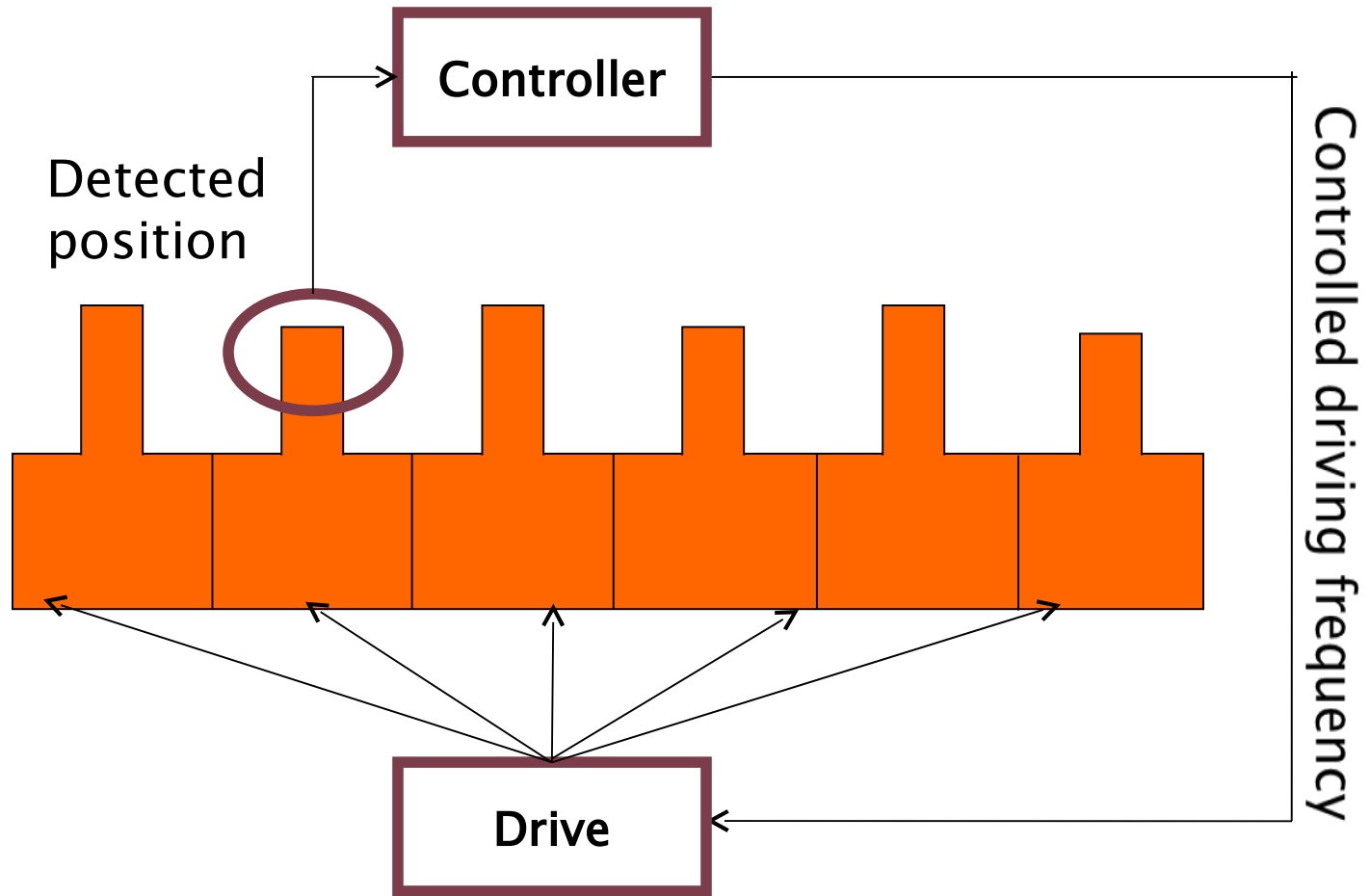


Creating ILMs from chaos

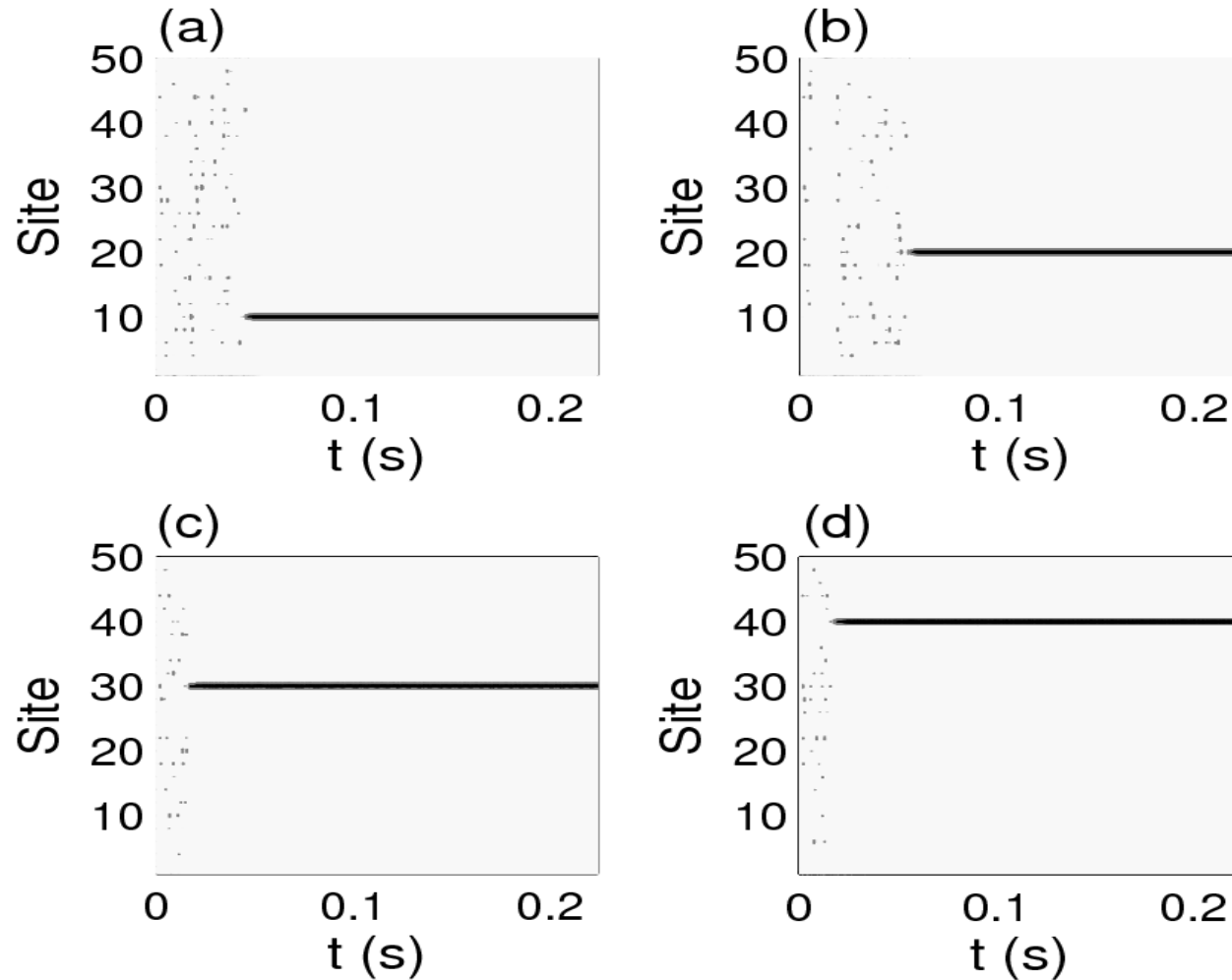


Creating ILMs from ST chaos

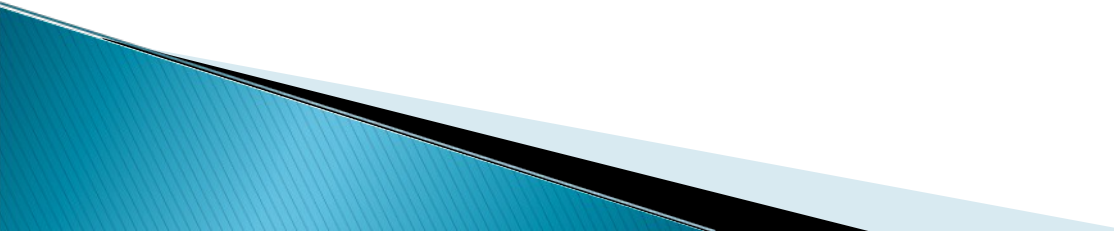




Different patterns in MEM array

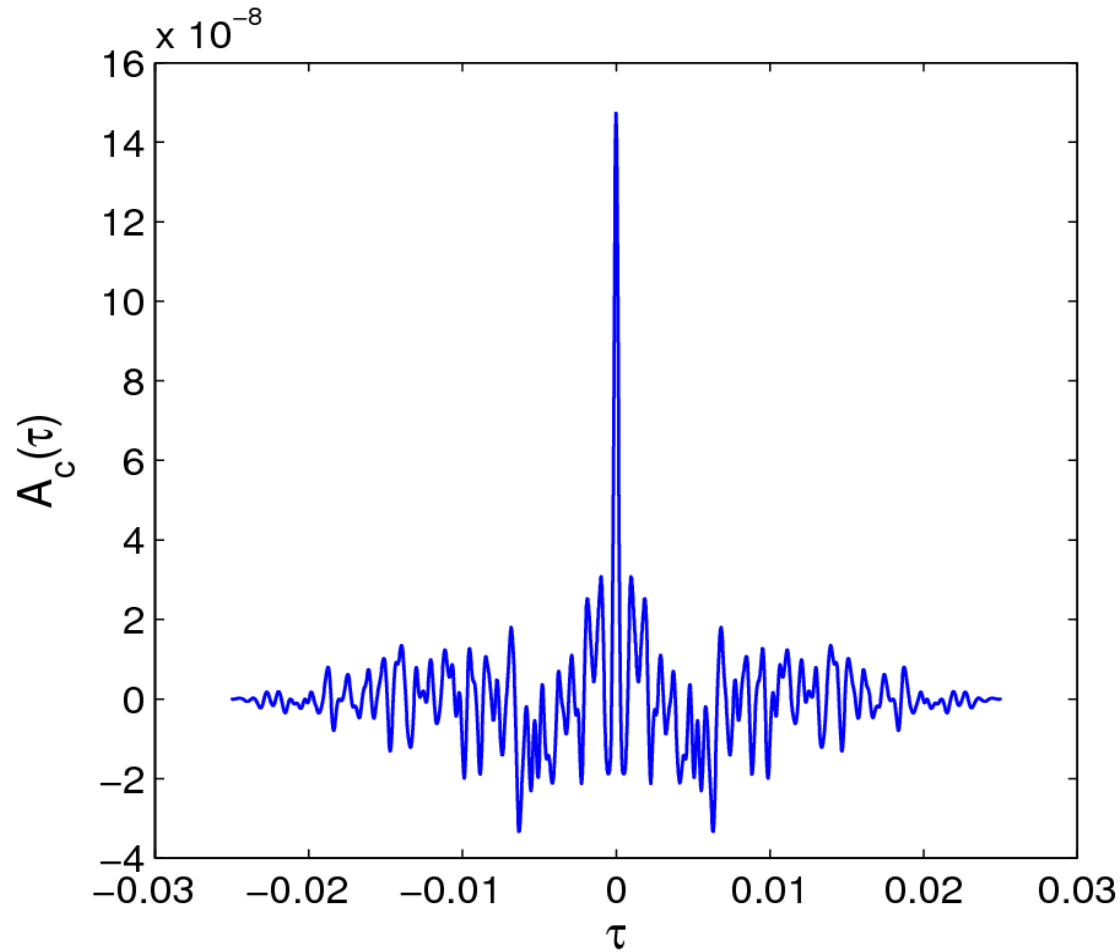


Conclusion

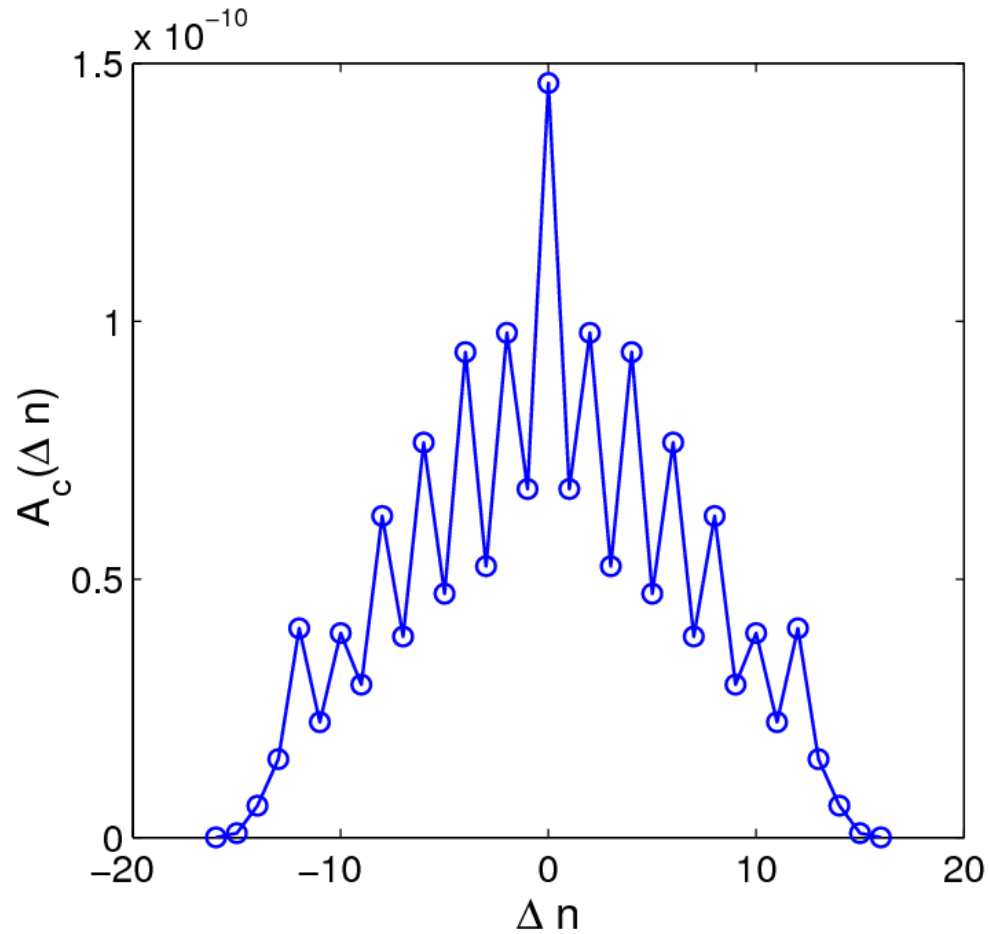
- ▶ An averaged model to study the dynamics of driven microcantilever arrays.
 - ▶ Spatiotemporal chaos serves as a natural exciting platform for ILMs.
 - ▶ Forming different patterns of ILMs in MEM cantilever arrays.
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Thanks!

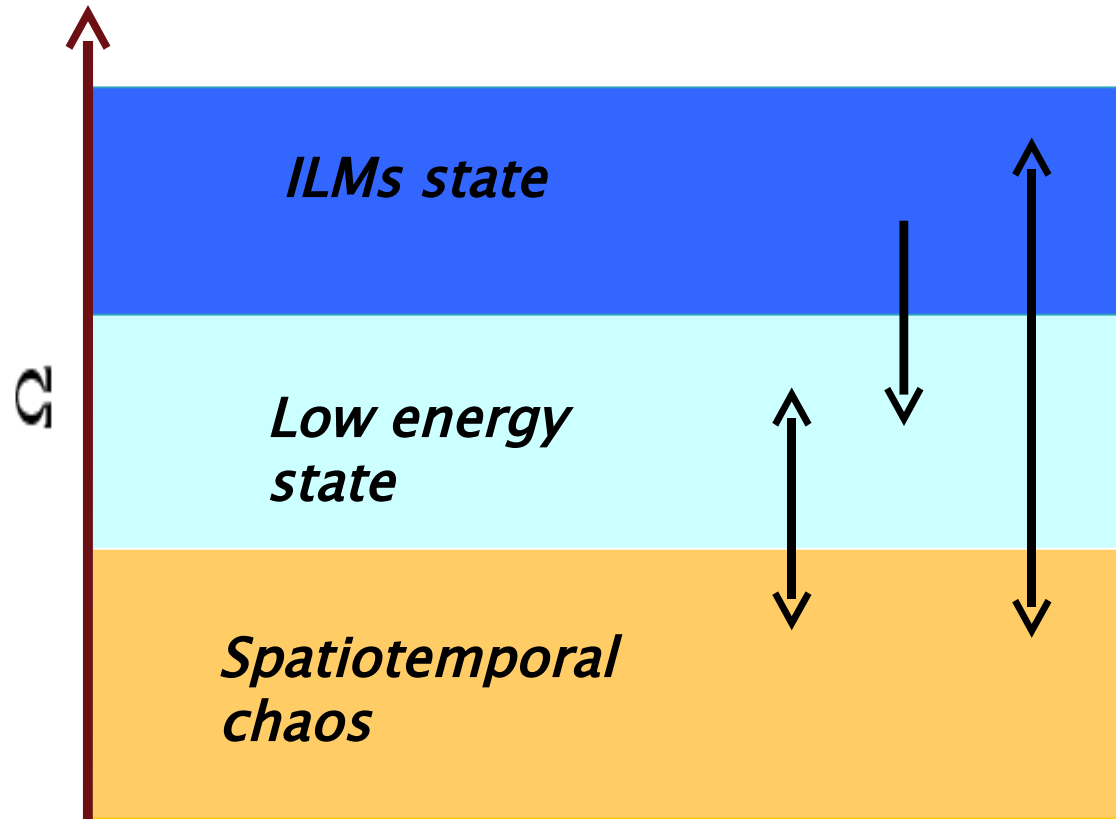
Correlation function of time



Correlation function in space



Creating ILMs from chaos



Controlled MEM arrays

$$m_i \ddot{x}_i + b_i \dot{x}_i + k_{2i} x_i + k_{4i} x_i^3 + k_I (2x_i - x_{i+1} - x_{i-1}) = m_i \alpha \cos(\Omega_c t), \text{ where } x_i \text{ (} i = 1, \dots, N \text{)}$$

$$\begin{cases} \dot{\Omega}_c = \gamma \xi \\ \dot{\xi} = -(1/\tau)(\xi + x_M \sin(\Omega_c t + \phi)) \end{cases}$$

Dynamic model of MEM arrays

MEM cantilever arrays equation:

$$m_i \ddot{x}_i + b_i \dot{x}_i + k_{2i} x_i + k_{4i} x_i^3 + k_I (2x_i - x_{i+1} - x_{i-1}) = m_i \alpha \cos(2\pi ft),$$

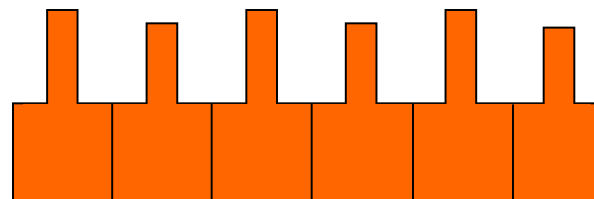
where x_i ($i = 1, 2 \dots N$) N is even

$$(m_i, b_i, k_{2i}, k_{4i}) = (m_a, b_a, k_{2a}, k_{4a}) \quad \text{if } i \text{ is odd}$$

$$(m_i, b_i, k_{2i}, k_{4i}) = (m_b, b_b, k_{2b}, k_{4b}) \quad \text{if } i \text{ is even}$$

m_i : mass

b_i : damping coefficient



Averaged model for MEM arrays

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$$\frac{du_i}{dt} = -\frac{1}{2\Omega} [(\Omega^2 - \Omega_{0i}^2)v_i - \frac{3}{4} \frac{k_{4i}}{m_i} v_i(u_i^2 + v_i^2) + \frac{\Omega_{0i}}{Q_i} \Omega u_i - \frac{k_I}{m_i} (2v_i - v_{i+1} - v_{i-1})],$$

$$\frac{dv_i}{dt} = \frac{1}{2\Omega} [(\Omega^2 - \Omega_{0i}^2)u_i - \frac{3}{4} \frac{k_{4i}}{m_i} u_i(u_i^2 + v_i^2) - \frac{\Omega_{0i}}{Q_i} \Omega v_i + \alpha - \frac{k_I}{m_i} (2u_i - u_{i+1} - u_{i-1})], \quad i = 1, \dots, N.$$

where $\Omega_{0i} = \sqrt{k_{2i}/m_i}$, $Q_i = \sqrt{m_i k_{2i}}/b_i$

u_i and v_i are the averaged functions of $U_i(t)$ and $V_i(t)$ over one period, respectively.

Amplitudes and phase angles can be approximated by:

$$A_i = \sqrt{u_i^2 + v_i^2}, \theta_i = \arctan(v_i/u_i)$$

